

CH6511 Process Equipment Design - I

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Mechanical Design of Chemical Process Equipments Pressure Vessel Design

Dr. M. Subramanian

Associate Professor

Department of Chemical Engineering

Sri Sivasubramaniya Nadar College of Engineering

Kalavakkam – 603 110, Kanchipuram (Dist)

Tamil Nadu, India

subramanianm@ssn.edu.in



Pressure Vessel Design

- ASME Section VIII is most widely used Code.
- Assures safe design.
- IS 2825 – Indian standard code

Materials of Construction

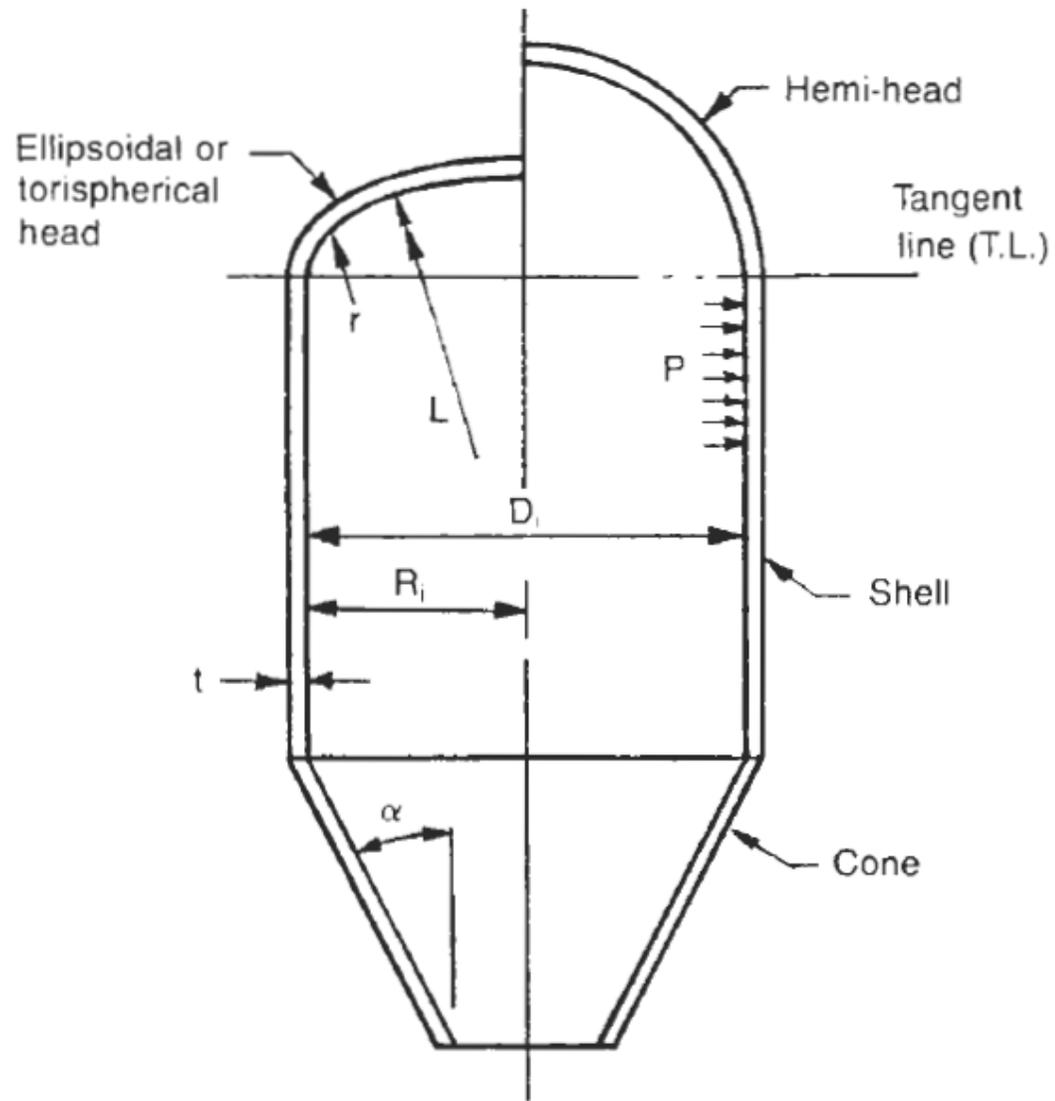
- Plate Materials:
 - Mild Steel: A-36, A-516 Gr 60, 70,
 - Stainless Steel: 304, 316, 304L, 316L
- Pipe Materials – A106,
- Forgings – A105,

SS 304	18 - 20 % Cr, 8 - 12 % Ni, 0.08% (max) C	18-8 stainless steel, most commonly used material for process equipments
SS 304L	18 - 20 % Cr, 8 - 12 % Ni, 0.03% (max) C	Low carbon version of SS 304
SS 316	16 - 18 % Cr, 10 - 14% Ni, 2 - 3 % Mo, 0.1% (max) C	Addition of molybdenum improves resistance to chloride environments.
SS 316L	16 - 18 % Cr, 10 - 14% Ni, 2 - 3 % Mo, 0.03% (max) C	Low carbon version of SS 316
SS 430	14 - 18 % Cr, 0.5% Ni	Tableware. The first chemical plant application of stainless steel was SS 430 tank-car for shipping nitric acid.

Titanium - wet chlorine: The industries like paper, textile, plastics and detergents, which use wet chlorine and bleaching agents have started using titanium equipment for extended life of their plant and equipment.

- Should not be used with dry chlorine

Nickel: Most tough corrosion problems involving caustic and caustic solutions are handled with nickel. Corrosion resistance to caustic is almost directly proportional to the nickel content of an alloy.



Thickness of Pressure Vessels

- Cylindrical vessel

- Longitudinal stress:

$$t = \frac{pd}{4fJ}$$

- Circumferential stress:

$$t = \frac{pd}{2fJ}$$

where t = thickness of shell
 d = diameter of cylinder
 p = design pressure
 f = allowable stress
 J = joint efficiency

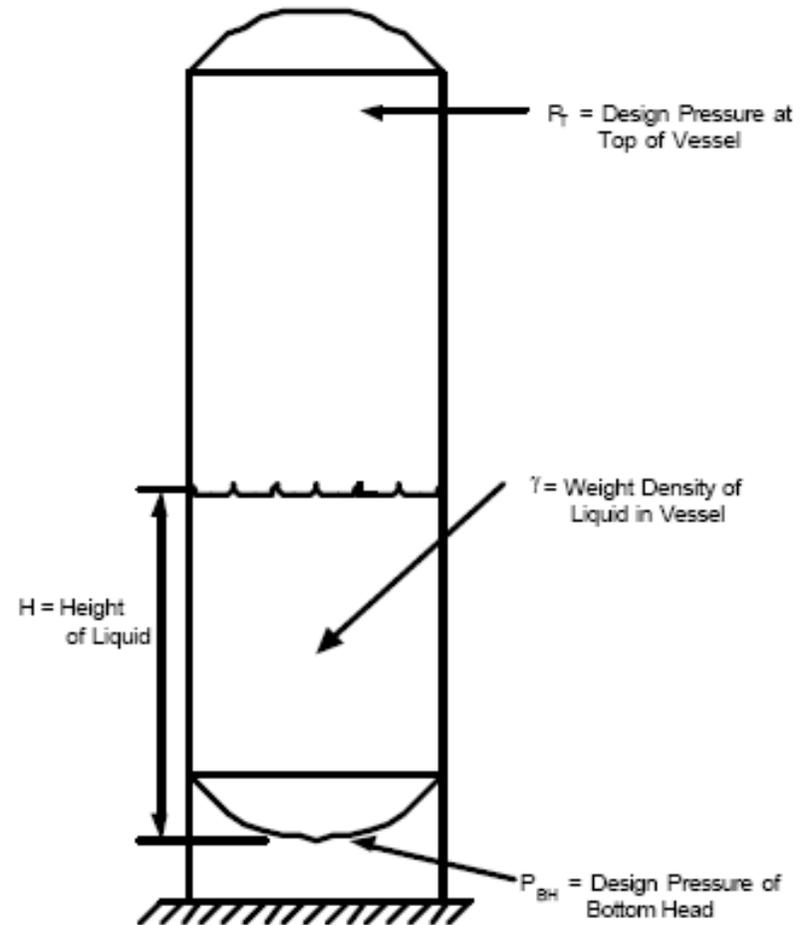
Circumferential stress is the controlling stress; and cylindrical shell is designed based on the circumferential stress formula.

- Spherical vessel

$$t = \frac{pd}{4fJ}$$

Design Pressure

- May have internal or external pressure, or both at different times.
- Must have margin between maximum operating pressure at top of vessel and design pressure.
- Hydrostatic pressure of operating liquid (if present) must be considered at corresponding vessel elevation.



Design Pressure

- For vessels under internal pressure, the design pressure is normally taken as the pressure at which the relief device is set. This will normally be 5 to 10 per cent above the normal working pressure, to avoid spurious operation during minor process upsets.
- Vessels subject to external pressure should be designed to resist the maximum differential pressure that is likely to occur in service.

Additional Loadings

Loadings other than pressure and temperature:

- Weight of vessel and normal contents under operating or test conditions
- Superimposed static reactions from weight of attached items (e.g., motors, machinery, other vessels, piping, linings, insulation)
- Loads at attached internal components or vessel supports
- Wind, snow, seismic reactions

Joint Efficiency

- 1, 0.85, 0.7

- **Joint Efficiency**

- No radiography : 70%

- Spot radiography : 85%

- 100% radiography : 100%

- Joint efficiency is 100% for seamless heads.

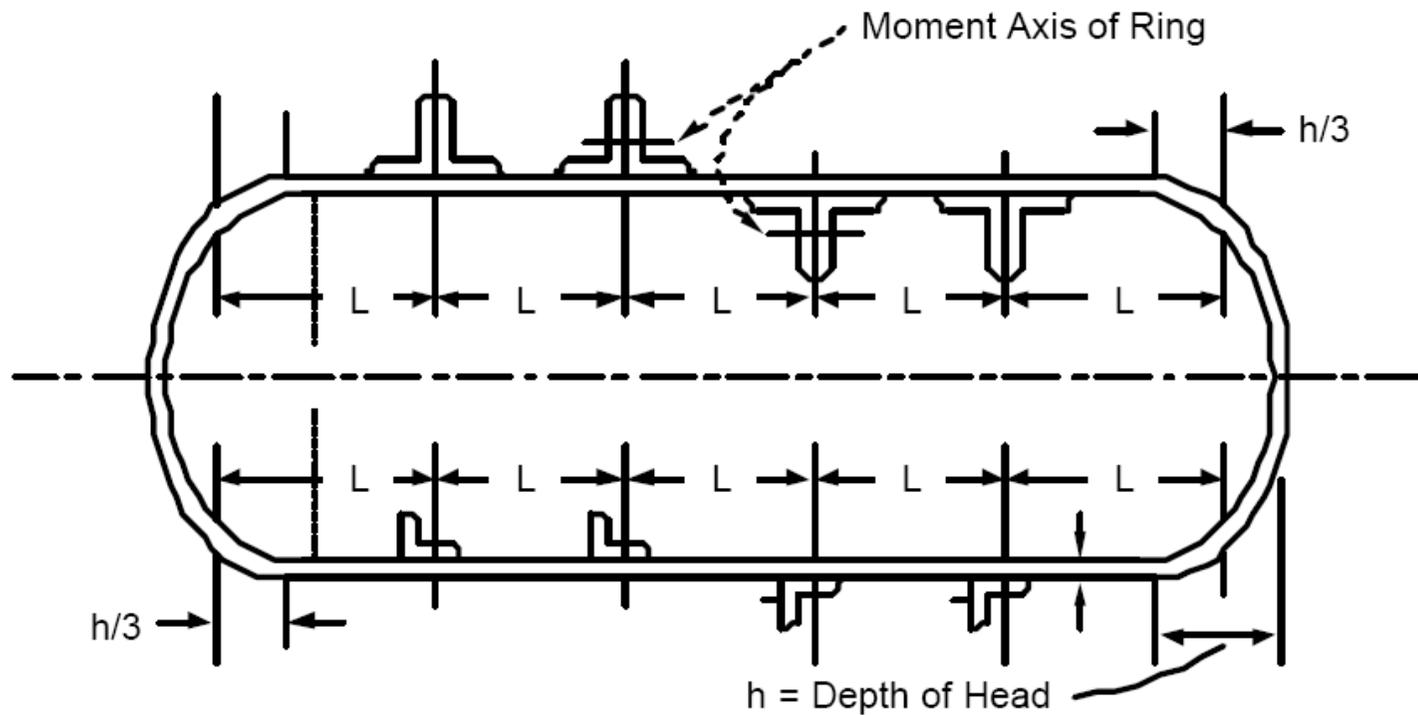
Corrosion Allowance

- The corrosion allowance must be added to the calculated thickness.

Design for External Pressure and Compressive Stresses

- Compressive forces caused by dead weight, wind, earthquake, internal vacuum
- Can cause elastic instability (buckling)
- Vessel must have adequate stiffness
 - Extra thickness
 - Circumferential stiffening rings

Stiffener Rings



Design for Internal Pressure

- Inside Diameter - 10' - 6"
- Design Pressure - 650 psig
- Design Temperature - 750°F
- Shell & Head Material - SA-516 Gr. 70
- Corrosion Allowance - 0.125 in.
- 2:1 Semi-Elliptical heads, seamless
- 100% radiography
- Vessel in vapor service

Design – as per codes

- For shell $t_p = \frac{Pr}{SE_1 - 0.6P}$

$P = 650$ psig

$r = 0.5 \times D + CA$

$= (0.5 \times 126) + 0.125 = 63.125$ in.

- $S = 16,600$ psi, Figure 3.3 for SA-516 Gr. 70

- $E = 1.0$, Figure 4.8 for 100% radiography

$$t_p = \frac{650 \times 63.125}{(16,600 \times 1.0) - (0.6 \times 650)} = 2.53 \text{ in.}$$

Add corrosion allowance

$$t_p = 2.53 + 0.125 = 2.655 \text{ in.}$$

- For the heads

$$t_p = \frac{PD}{2SE - 0.2P}$$

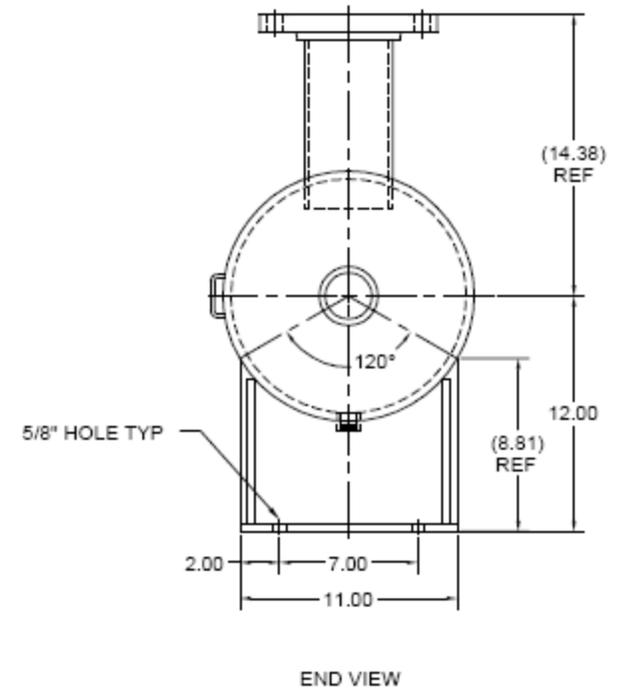
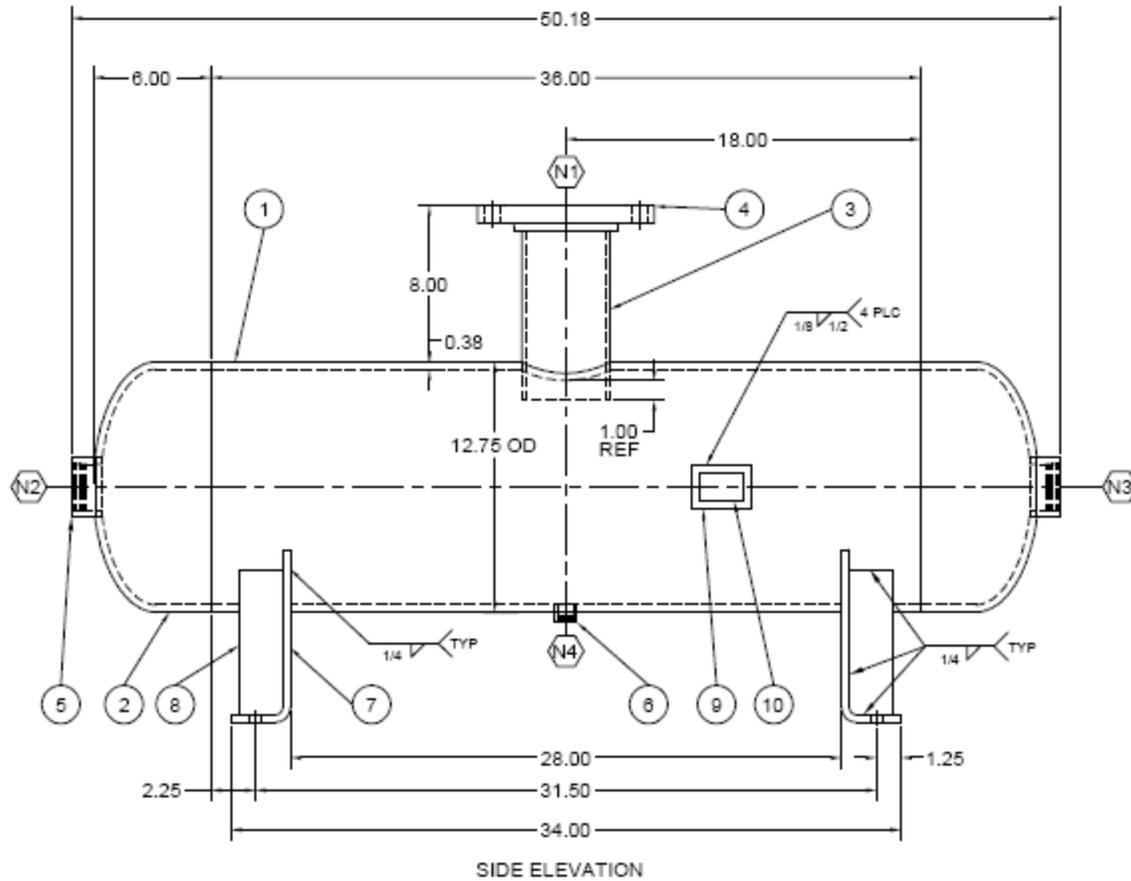
$$t_p = \frac{650(126 \times 0.9) + 0.250}{(2 \times 16,600) - (0.2 \times 650)} = 2.23 \text{ in.}$$

Add corrosion allowance

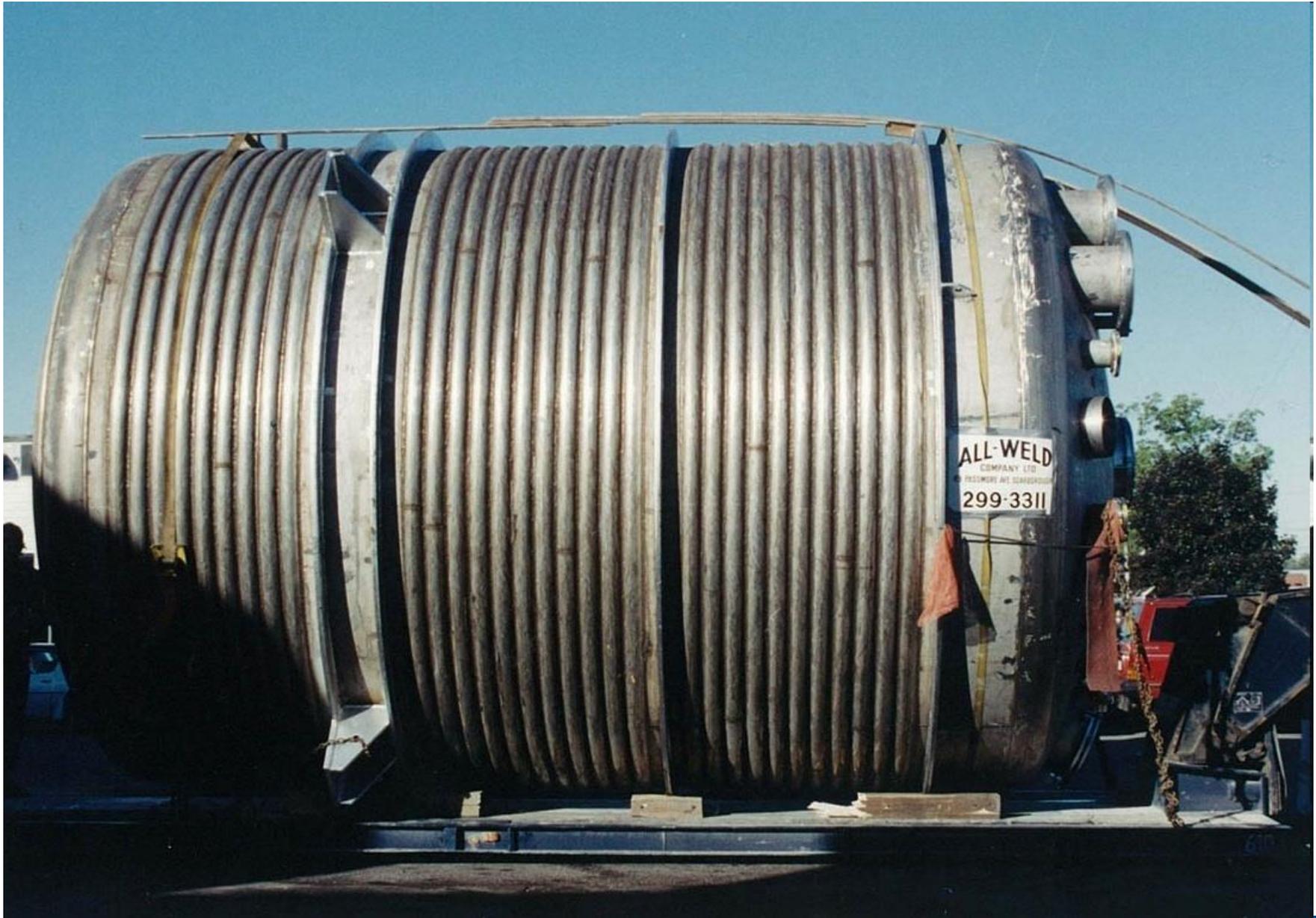
$$t_p = 2.23 + 0.125 = 2.355 \text{ in.}$$

Design Codes

- Pressure Vessels: ASME Sec VIII, IS 2825
- Storage Tank: API 650, IS 803







Storage Tanks









